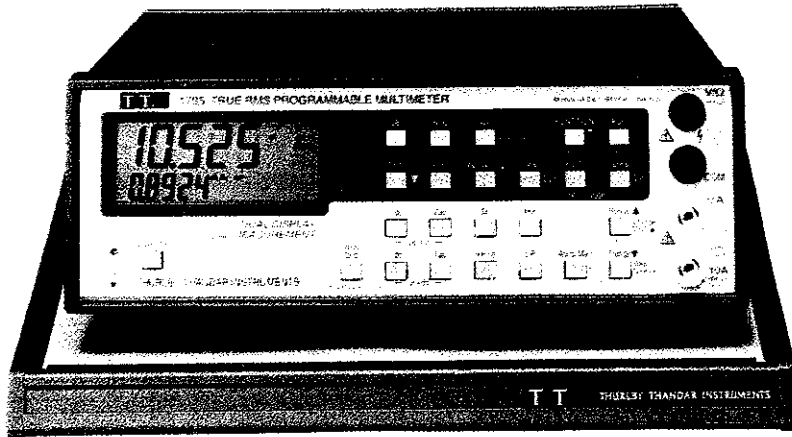


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Frequency-programmable analogue band-pass filter

Centre frequency of this filter is linearly proportional to the digital inputs of an a-to-d R-2R ladder converter. Two main elements comprise the circuit: a gyrator and a band-pass filter. Figure 1 shows the gyrator, the input

impedance of which is given by,

$$z_{in}(s) = sR_1R_2$$

which appears as an equivalent inductor with a value of $L_{eq} = LR_1R_2$.

Figure 2 is a basic band-pass filter, whose transfer function is,

$$H(s) = s/CR' / (s^2 + s/CR' + 1/LC)$$

compared with that of a second-order band-pass, which is,

$$H(s) = \omega_0 A_0 s / Q(s^2 + s\omega_0/Q + \omega_0^2)$$

Pass-band gain is 1 and centre frequency

$$f_0 = 1/(2\pi LC) = \omega_0 / 2\pi$$

$$\text{Bandwidth is } f_0 / Q = 1/(2\omega_0 CR)$$

An analogue-to-digital converter is represented in Fig. 3, in which $b_{n-1}, b_{n-2} \dots b_0$ are the digital inputs to an n-bit R-2R

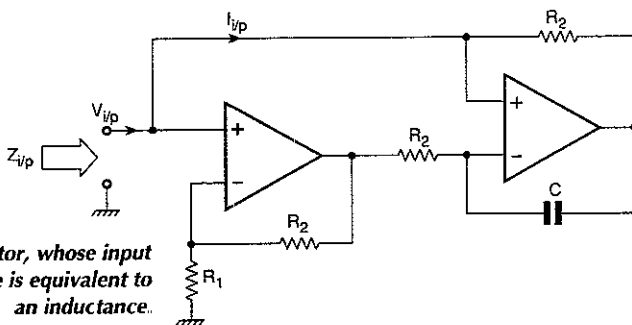


Fig. 1. A gyrator, whose input impedance is equivalent to an inductance.

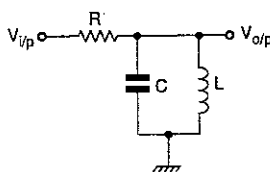


Fig. 2. Band-pass filter.

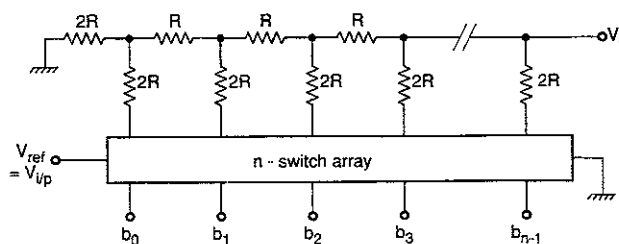


Fig. 3. N-bit ladder network used in an analogue-to-digital converter, the input voltage being represented by the resistor switches.

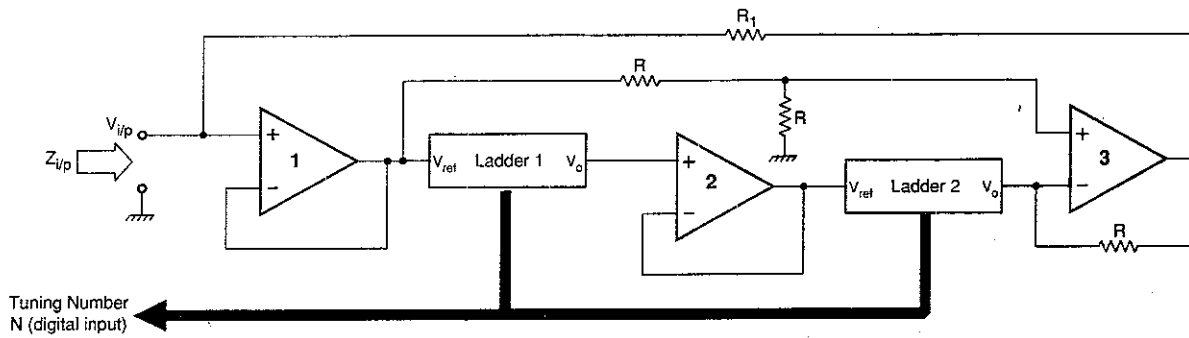


Fig. 4. Input impedance of this arrangement is resistive and varying inversely with N^2 .

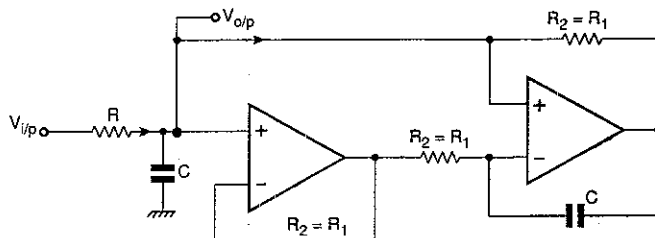
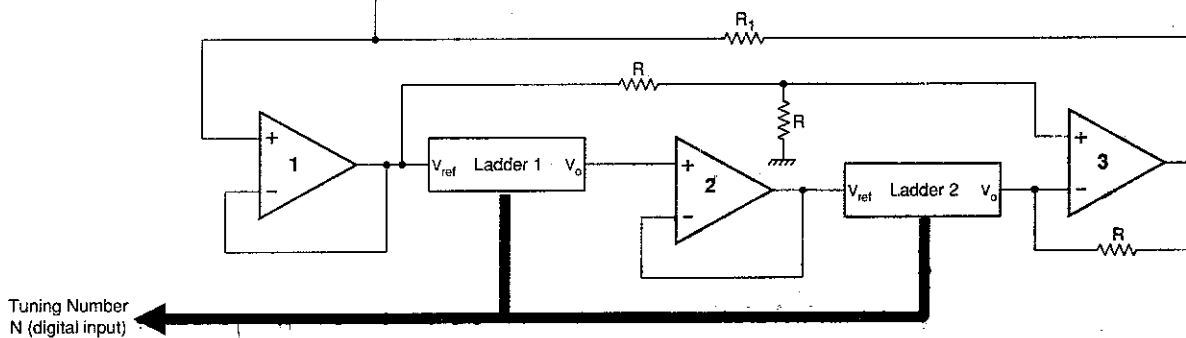


Fig. 5. Complete circuit of programmable band-pass filter. Maximum frequency is set by op-amp slewing rate. The ladders may be replaced by d-to-a converter ics,



ladder network, whose output is $v_o = N/2^n v_{in}$. Output impedance is R .

Figure 4 is a development of this, in which the op-amps are simply buffers and both ladders have the same digital input. Output voltage of ladder 1 is $(N/2^n)v_{in}$, which is also the input to ladder 2, whose output is therefore $(N/2^n)^2 v_{in}$. The output impedance of the ladders being R , op-amp 3 output voltage is Av_{in} .

Now connecting R_1 from input to output produces an input impedance,

$$z_{in} = R_1 / (1 - A) = R_1 / (1 - (1 - N/2^n)^2) = R_1 (2^n / N)^2$$

which is a resistance varying inversely as the square of N .

If now the resistor R_1 in the gyrator circuit of Fig 1 is replaced with the circuit of Fig 3 and this new gyrator is used as the inductor in the circuit of Fig 2, the whole being shown in Fig 4, the centre frequency becomes,

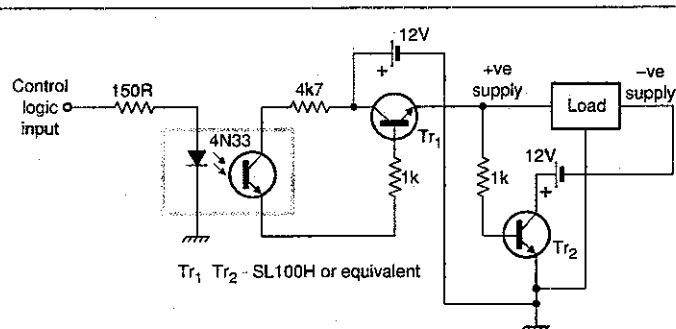
$$f_0 = 1 / (2\pi(R_2 R_1 (2^n / N)^2 - C)^{1/2})$$

$$\text{If } R_2 = R_1,$$

$$f_0 = N / (2\pi R_1 C * 2^n),$$

the centre frequency being proportional to the tuning number N , independently of bandwidth.

S. Santhosh Kumar
Kerala
India



Both rails of a dual power supply are switched by logic input.

Switch two supply rails at once, digitally

Logic-level signals control the on/off switching of dual power supplies.

Input switching logic signals go to an opto-isolator which, when conducting, supplies base current to Tr_1 and completes the path from the +12V supply through the load to ground. At the same time, Tr_2 receives base current via Tr_1 and provides the path for the negative 12V supply. In the absence of drive to the opto-isolator, both transistors are off and neither power supply is connected.

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