MATCHING NETWORK DESIGNS WITH COMPUTER SOLUTIONS

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INTRODUCTION

One of the problems facing the circuit design engineer is the design of high-frequency matching networks. Careful design of a network that will accomplish the required matching, harmonic attenuation, bandwidth, etc., and yield components of practical size can result in many hours spent with pencil and slide rule.

The design of matching networks for high frequency circuits involves an infinite number of possibilities, and a complete tabulation of possible network solutions would be virtually impossible. However, it is often necessary to design matching networks with a 50 + j 0 ohm impedance at one port. This, combined with a restricted range of impedance values to be matched, imposed by network and device limitations, makes practical a tabulation of some of the more commonly used networks. These design solutions are given in this report.

The network solutions included in this report have the limitation that one terminating impedance must be 50 + j 0 ohms. These networks are often used for matching in transistor RF power amplifier circuits that have a 50-ohm source or load. When the network does not have a 50-ohm termination at either port, the mathematical procedure given for each network in Appendix I can be used for the solution.

COMPONENT CONSIDERATIONS

Four networks are presented in this report with solutions in the form of computer tabulations. Each network has its own limitations. Although the network configuration is normally up to the discretion of the design engineer, it is sometimes necessary to use one configuration in preference to another in order to obtain component values that are more realistic from a practical standpoint.

Component selection in the UHF and VHF frequency ranges becomes a major problem, and the network configuration to obtain realistic component values is of vital importance to the design engineer. Design calculations for matching networks can become completely meaningless unless the components for the network are measured at the operating frequency.

For example, a 100 pF silver mica capacitor that meets all specifications at 1 MHz can have as much capacitance as 300 pF at 100 MHz. At some frequency, the capacitor's series lead inductance will finally tune out the capacitance, thus leaving the capacitor net inductive.

Values of inductance in the low nanohenry range are also difficult to obtain, since the inductance of a one-inch straight piece of #20 solid tinned wire is approximately 20 nH.

Component tolerances have no meaning at VHF frequencies and above unless they are specified at the operating frequency. It cannot be over-emphasized that components must be measured at the operating frequency.

NETWORK SOLUTIONS

The resistor and capacitor shown in the box labeled "device to be matched" represent the complex input or output impedance of a transistor. These complex impedances have been represented in series form in some cases and parallel form in others, depending on which form is most convenient for network calculation. The resultant impedance of the network, when terminated with 50 + j 0 ohms, must be equal to the conjugate of the impedance in the box. The computer tabulations provide this solution.

Network A (see Figure 1) is applicable only when the "device to be matched" has a series real part of less than 50 ohms. As we can see from the computer tabulation, as the series real part approaches 50 ohms, the reactance of C_1 approaches infinity. However, in RF power amplifiers, we normally find that the series real part of both the input and the output is less than 50 ohms, making this matching network applicable to most RF power amplifier stages. Where the terminating impedance is other than 50 ohms, the mathematical procedure for the network solution is given in Appendix I.

Network B (see Figure 2) is the Pi network widely used in vacuum tube transmitters. As is apparent from the computer tabulation, this network is often impractical for use where R_1 is small. For values of R_1 less than 50 ohms, the inductance of L becomes impractically small while the capacitance of both C_1 and C_2 become very large. Where the Pi network configuration must be used to match low values of impedance, a double Pi network, in which the Q of the first section is very low, can be utilized to yield practical components.

Network C has been solved in two forms (see Figure 3). Both of these networks have the limitation that R_1 must be less than 50 ohms. However, it must be stressed that this network configuration quite often yields the most practical components where low values of R_1 must be matched.

Network D (see Figure 4) is a "Tee" network. This network is useful for matching impedance less than or greater than 50 ohms. It has been observed in laboratory tests that this network configuration also yields very high collector efficiencies when used for output matching in transistor RF power amplifier stages.

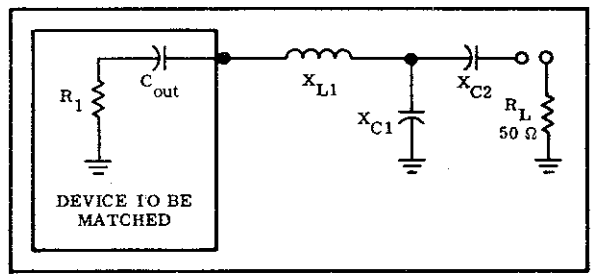


FIGURE 1 — NETWORK A

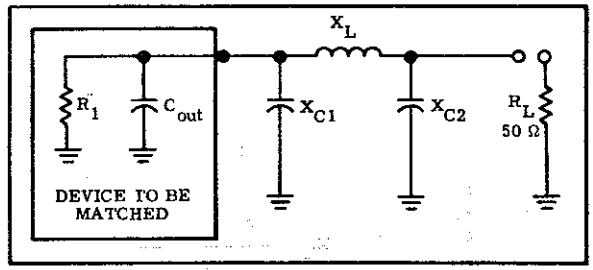


FIGURE 2 — NETWORK B

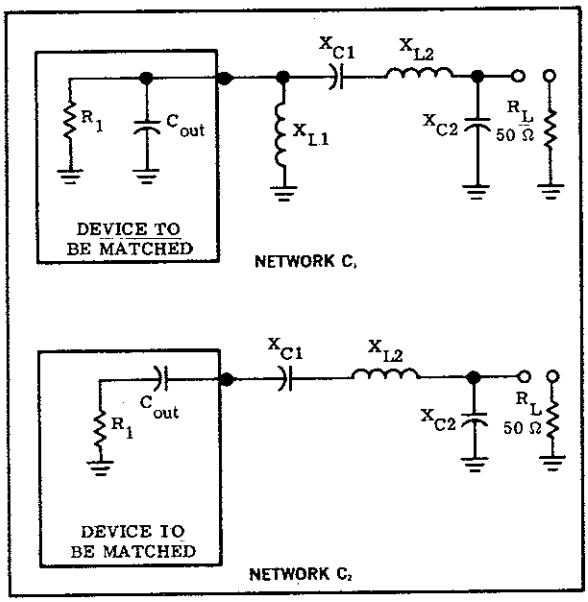


FIGURE 3

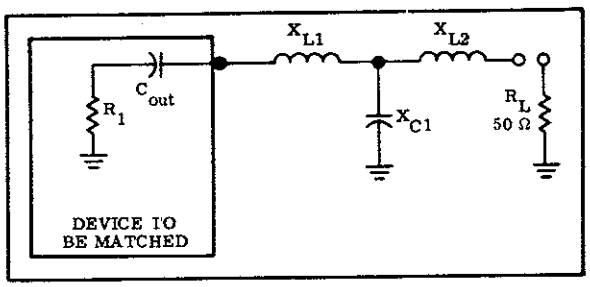


FIGURE 4 — NETWORK D

SUMMARY

Four computer-solved networks have been presented. The mathematical procedure for the solution of each network has been given in Appendix I.* Although the networks have found major use in matching solid-state RF power amplifier stages, they are also applicable to any circuit where the individual network's limitations are fulfilled.

*For the derivation of the equations used, refer to Electronic Circuit Analysis, Volume 1, "Passive Networks," Philip Cutler.

APPENDIX I

To convert a parallel resistance and reactance combination to series:

$$R_s = \frac{R_P}{1 + (R_P/X_P)^2}$$

$$X_s = R_s \frac{R_P}{X_P}$$

To convert a series resistance and reactance combination to parallel:

$$R_P = R_s[1 + (X_s/R_s)^2]$$

$$X_P = \frac{R_P}{X_s/R_s}$$

To solve network A:

1. Select a Q

$$X_{L1} = QR_1 + X_{C\,out}$$

$$X_{C2} = AR_L$$

$$X_{C1} = \frac{(B/A)(B/Q)}{(B/A)-(B/Q)} = \frac{B}{Q - A}$$

where $A = \sqrt{\left[\frac{R_1(1+Q^2)}{R_L}\right] - 1}$

$$B = R_1(1 + Q^2)$$

To solve network B:

1. Select a Q

$$X_{C1} = R_1/Q$$

$$X_{C2} = R_L\sqrt{\frac{R_1/R_L}{(Q^2+1)-(R_1/R_L)}}$$

$$X_L = \frac{QR_1 + (R_1R_L/X_{C2})}{Q^2 + 1}$$

To solve network C_1:

1. Select a Q

$$X_{L1} = X_{C\,out}$$

$$X_{C1} = QR_1$$

$$X_{C2} = R_L\sqrt{\frac{R_1}{R_L - R_1}}$$

$$X_{L2} = X_{C1} + \left(\frac{R_1R_L}{X_{C2}}\right)$$

To solve network C_2:

1. Select a Q
2. L_1 is not used in this network

$$X_{C1} = QR_1$$

$$X_{C2} = R_L\sqrt{\frac{R_1}{R_L - R_1}}$$

$$X_{L2} = X_{C1} + \left(\frac{R_1R_L}{X_{C2}}\right) + X_{C\,out}$$

To solve network D:

1. Select a Q

$$X_{L1} = (R_1Q) + X_{C\,out}$$

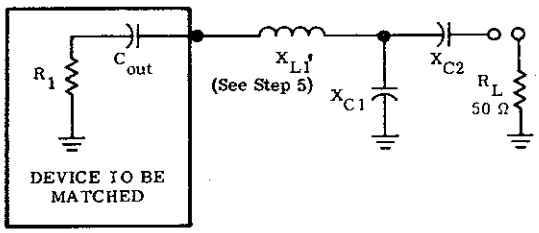
$$X_{L2} = R_LB$$

$$X_{C1} = \frac{(A/Q)(A/B)}{(A/Q) + (A/B)} = \frac{A}{Q + B}$$

where $A = R_1(1 + Q^2)$

$$B = \sqrt{\left(\frac{A}{R_L}\right) - 1}$$

NETWORK A



TO DESIGN A NETWORK USING THE TABLES

1. Transform the parallel impedance of the device to be matched to series form ($R_1 + jX_{C_{out}}$)
2. Define Q, in column one, as X_{L1}/R_1.
3. Choose a Q.
4. For a Q, find the R_s to be matched in the R column and read the reactive value of the components.
5. X_{L1}' is equal to the quantity X_{L1} obtained from the tables plus $|X_{C_{out}}|$.
6. This completes the network.

Q	X_{L1}	X_{C1}	X_{C2}	R_1
1	26	65	10	26
1	27	75.3	14.14	27
1	28	85.68	17.32	28
1	29	96.66	20	29
1	30	108.5	22.36	30
1	32	136	26.46	32
1	34	170	30	34
1	36	213.8	33.16	36
1	38	272.5	36.05	38
1	40	355	38.7	40
1	42	479	41.23	42
1	44	686.32	43.59	44
1	46	1102	45.83	46
1	48	2351	48	48
2	22	32.7	15.8	11
2	24	38.6	22.4	12
2	26	45	27.4	13
2	28	51.2	31.6	14
2	30	58	35.4	15
2	32	65.3	38.7	16
2	34	73.1	41.8	17
2	36	81.4	44.7	18
2	38	90.3	47.4	19
2	40	100	50	20
2	42	110.4	52.4	21
2	44	122	55	22
2	46	134	57	23
2	48	147	59	24
2	50	161	61	25
2	52	177	63	26
2	54	194	65	27
2	56	213	67	28
2	58	233	69	29
2	60	256	71	30
2	64	310	74	32
2	68	377	77	34
2	72	464	81	36
2	76	582	84	38
2	80	746	87	40
2	84	995	89	42
2	88	1409	92	44
2	92	2241	95	46
2	96	4739	97	48
3	18	23.5	22.3	6
3	21	29.6	31.6	7
3	24	35.9	38.7	8
3	27	42.7	44.7	9
3	30	50	50	10
3	33	57.8	54.8	11
3	36	66	59	12
3	39	75	63.2	13

Q	X_{L1}	X_{C1}	X_{C2}	R_1
3	42	84	67	14
3	45	95	71	15
3	48	105	74	16
3	51	117	77	17
3	54	130	81	18
3	57	143	84	19
3	60	158	87	20
3	63	173	89	21
3	66	190	92	22
3	69	209	95	23
3	72	228	97	24
3	75	250	100	25
3	78	274	102	26
3	81	299	105	27
3	84	327	107	28
3	87	358	110	29
3	90	393	112	30
3	96	473	116	32
3	102	575	120	34
3	108	706	124	36
3	114	882	128	38
3	120	1129	132	40
3	126	1502	136	42
3	132	2124	140	44
3	138	3372	143	46
3	144	7119	146	48
4	12	13.2	7.1	3
4	16	20	30	4
4	20	26.9	41.8	5
4	24	34.2	51	6
4	28	42.1	58.7	7
4	32	50.6	66	8
4	36	60	72	9
4	40	69	77	10
4	44	80	83	11
4	48	91	88	12
4	52	103	92	13
4	56	115	97	14
4	60	129	101	15
4	64	144	105	16
4	68	159	109	17
4	72	176	113	18
4	76	194	117	19
4	80	214	120	20
4	84	235	124	21
4	88	257	127	22
4	92	282	131	23
4	96	308	134	24
4	100	337	137	25
4	104	368	140	26
4	108	403	143	27

Q	X_{L1}	X_{C1}	X_{C2}	R_1
4	112	440	146	28
4	116	482	149	29
4	120	527	152	30
4	128	635	157	32
4	136	770	162	34
4	144	945	168	36
4	152	1180	173	38
4	160	1510	177	40
4	168	2007	182	42
4	176	2837	187	44
4	184	4500	191	46
4	192	9497	196	48
5	10	10.8	10	2
5	15	18.3	37.4	3
5	20	26.3	52	4
5	25	34.8	63.2	5
5	30	44	73	6
5	35	54	81	7
5	40	65	89	8
5	45	76	96	9
5	50	88	102	10
5	55	101	108	11
5	60	115	114	12
5	65	130	120	13
5	70	146	125	14
5	75	163	130	15
5	80	181	135	16
5	85	201	140	17
5	90	222	145	18
5	95	245	149	19
5	100	269	153	20
5	105	295	157	21
5	110	323	162	22
5	115	354	166	23
5	120	387	169	24
5	125	423	173	25
5	130	462	177	26
5	135	505	181	27
5	140	553	184	28
5	145	604	188	29
5	150	662	191	30
5	160	796	198	32
5	170	965	204	34
5	180	1184	210	36
5	190	1477	217	38
5	200	1890	222	40
5	210	2510	228	42
5	220	3548	234	44
5	230	5628	239	46
5	240	11874	245	48

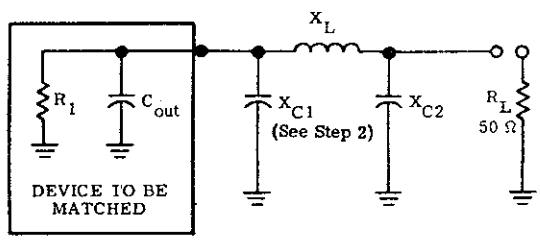
Q	X_{L1}	X_{C1}	X_{C2}	R_1
6	12	13.9	34.6	2
6	18	22.7	55.2	3
6	24	32.2	70	4
6	30	42.5	82	5
6	36	53.6	93	6
6	42	65.5	102	7
6	48	78	110	8
6	54	92	119	9
6	60	107	126	10
6	66	122	133	11
6	72	139	140	12
6	78	157	147	13
6	84	176	153	14
6	90	197	159	15
6	96	219	165	16
6	102	242	170	17
6	108	267	175	18
6	114	295	181	19
6	120	324	186	20
6	126	355	191	21
6	132	389	195	22
6	138	426	200	23
6	144	466	205	24
6	150	509	209	25
6	156	556	214	26
6	162	608	218	27
6	168	664	222	28
6	174	727	226	29
6	180	795	230	30
6	192	957	238	32
6	204	1160	246	34
6	216	1422	253	36
6	228	1775	260	38
6	240	2270	267	40
6	252	3015	274	42
6	264	4260	281	44
6	276	6755	287	46
6	288	14250	294	48
7	14	16.7	50	2
7	21	26.8	71	3
7	28	38	87	4
7	35	50	100	5
7	42	63	112	6
7	49	77	122	7
7	56	92	132	8
7	63	108	141	9
7	70	125	150	10
7	77	143	158	11
7	84	163	166	12
7	91	184	173	13
7	98	206	180	14
7	105	230	187	15
7	112	256	193	16
7	119	283	200	17
7	126	313	206	18
7	133	344	212	19
7	140	379	218	20
7	147	415	224	21
7	154	455	229	22
7	161	498	234	23
7	168	544	239	24
7	175	595	245	25
7	182	650	250	26

Q	X_{L1}	X_{C1}	X_{C2}	R_1
7	189	710	255	27
7	196	776	260	28
7	203	849	265	29
7	210	929	269	30
7	224	1117	278	32
7	238	1354	287	34
7	252	1661	296	36
7	266	2071	304	38
7	280	2649	312	40
7	294	3518	320	42
7	308	4971	328	44
7	322	7882	335	46
7	336	16626	343	48
8	8	8.7	27.4	1
8	16	19.3	63.2	2
8	24	31	85	3
8	32	43.6	102	4
8	40	57.4	117	5
8	48	72	130	6
8	56	88	142	7
8	64	105	153	8
8	72	124	164	9
8	80	143	173	10
8	88	164	182	11
8	96	187	191	12
8	104	211	199	13
8	112	236	207	14
8	120	264	215	15
8	128	293	222	16
8	136	324	230	17
8	144	358	237	18
8	152	394	243	19
8	160	433	250	20
8	168	475	256	21
8	176	521	263	22
8	184	570	269	23
8	192	623	275	24
8	200	681	281	25
8	208	744	286	26
8	216	812	292	27
8	224	888	297	28
8	232	971	303	29
8	240	1062	308	30
8	256	1277	318	32
8	272	1548	329	34
8	288	1899	338	36
8	304	2368	348	38
8	320	3028	357	40
8	336	4022	366	42
8	352	5682	375	44
8	368	9009	383	46
9	9	10	40	1
9	18	21.9	76	2
9	27	35	99	3
9	36	49.4	118	4
9	45	65	134	5
9	54	82	149	6
9	63	100	162	7
9	72	119	174	8
9	81	139	185	9
9	90	162	196	10
9	99	185	206	11

Q	X_{L1}	X_{C1}	X_{C2}	R_1
9	108	210	216	12
9	117	237	225	13
9	126	266	234	14
9	135	297	243	15
9	144	330	251	16
9	153	365	259	17
9	162	403	267	18
9	171	444	275	19
9	180	488	282	20
9	189	535	289	21
9	198	586	296	22
9	207	641	303	23
9	216	701	310	24
9	225	766	316	25
9	234	837	323	26
9	243	914	329	27
9	252	999	335	28
9	261	1092	341	29
9	270	1196	347	30
9	288	1438	359	32
9	306	1743	370	34
9	324	2137	381	36
9	342	2665	391	38
9	360	3407	402	40
9	378	4525	412	42
9	396	6393	422	44
10	10	11.2	50.5	1
10	20	24.5	87	2
10	30	39	112	3
10	40	55	133	4
10	50	72	151	5
10	60	91	167	6
10	70	111	181	7
10	80	132	195	8
10	90	155	207	9
10	100	180	219	10
10	110	206	230	11
10	120	234	241	12
10	130	264	251	13
10	140	296	261	14
10	150	330	271	15
10	160	367	280	16
10	170	406	289	17
10	180	448	297	18
10	190	494	306	19
10	200	543	314	20
10	210	595	322	21
10	220	652	330	22
10	230	713	337	23
10	240	780	345	24
10	250	852	352	25
10	260	930	359	26
10	270	1016	366	27
10	280	1111	373	28
10	290	1214	379	29
10	300	1329	383	30
10	320	1598	399	32
10	340	1937	411	34
10	360	2375	423	36
10	380	2961	435	38
10	400	3787	446	40
10	420	5029	458	42
10	440	7104	469	44

NETWORK B

The following is a computer solution for the Pi network when R_L equals 50 ohms



TO DESIGN A NETWORK USING THE TABLES

1. Define Q, in column one, as R_1/X_{C1}
2. C_1 actual is equal to C_1 – parallel C_{out} of device to be matched.
3. This completes the network.

Q	X_{C1}	X_{C2}	X_L	R_1
1	1	5 03	5.47	1
1	2	7.14	8	2
1	3	8 79	10.03	3
1	4	10 21	11.8	4
1	5	11.47	13.4	5
1	10	16 67	20	10
1	15	21	25.35	15
1	20	25	30	20
1	25	28.87	34.15	25
1	30	32 73	37.91	30
1	35	36.69	41.35	35
1	40	40.82	44.49	40
1	45	45.23	47.37	45
1	50	50	50	50
1	55	55.28	52.37	55
1	60	61 24	54.49	60
1	65	68.14	56.35	65
1	70	76.38	57.91	70
1	75	86.6	59.15	75
1	80	100	60	80
1	85	119.02	60 35	85
1	90	150	60	90
2	0.5	3.17	3 56	1
2	1	4 49	5 25	2
2	1.5	5.51	6 64	3
2	2	6.38	7.87	4
2	2.5	7.14	9	5
2	5	10.21	13 8	10
2	7.5	12.63	17 87	15
2	10	14.74	21 56	20
2	12.5	16 67	25	25
2	15	18.46	28 25	30
2	17.5	20.17	31 35	35
2	20	21 82	34 33	40
2	22.5	23 43	37 21	45
2	25	25	40	50
2	27.5	26 55	42.71	55
2	30	28 1	45.35	60
2	32.5	29 64	47.93	65
2	35	31 18	50.45	70
2	37.5	32.73	52.91	75
2	40	34 3	55.32	80
2	42.5	35.89	57.69	85
2	45	37.5	60	90
2	47.5	39.14	62.27	95
2	50	40.82	64.49	100
2	62.5	50	75	125
2	75	61.24	84.49	150
2	87.5	76.38	92.91	175
2	100	100	100	200
2	112.5	150	105	225

Q	X_{C1}	X_{C2}	X_L	R_1
3	0.33	2.24	2.53	1
3	0.67	3 17	3 76	2
3	1	3.88	4.76	3
3	1.33	4 49	5.65	4
3	1 67	5 03	6.47	5
3	3.33	7.14	10	10
3	5	8.79	13.03	15
3	6.67	10.21	15.8	20
3	8.33	11.47	18.4	25
3	10	12.63	20.87	30
3	11.67	13.72	23.26	35
3	13 33	14.74	25.56	40
3	15	15.72	27 81	45
3	16.67	16.67	30	50
3	18.33	17.58	32 14	55
3	20	18 46	34.25	60
3	21.67	19 33	36.32	65
3	23.33	20 17	38 35	70
3	25	21	40 35	75
3	26.67	21 82	42 33	80
3	28.33	22 63	44 28	85
3	30	23.43	46.21	90
3	31.67	24.22	48 12	95
3	33.33	25	50	100
3	41.67	28.87	59 12	125
3	50	32 73	67 91	150
3	58 33	36.69	76 35	175
3	66.67	40.82	84 49	200
3	75	45.23	92.37	225
3	83 33	50	100	250
4	6.25	8.7	14 33	25
4	12.5	12.5	23 53	50
4	18.75	15 55	31.83	75
4	25	18.26	39.64	100
4	31.25	20.76	47.12	125
4	37.5	23.15	54.36	150
4	43.75	25.46	61.39	175
4	50	27.74	68 27	200
4	56.25	30	75	225
4	62.5	32.27	81.61	250
4	75	36.93	94 48	300
4	100	47.14	119.07	400
4	125	59 76	142 25	500
4	150	77 46	163.96	600
4	175	108.01	183 77	700
4	200	200	200	800
5	0.2	1.39	1.58	1
5	5	7	11 67	25
5	10	10	19.23	50
5	15	12.37	26.08	75

Q	X_{C1}	X_{C2}	X_L	R_1
5	20	14.43	32.55	100
5	25	16.31	38.78	125
5	30	18.06	44.82	150
5	35	19 72	50.72	175
5	40	21 32	56.5	200
5	45	22.87	62.18	225
5	50	24.4	67.78	250
5	60	27.39	78.76	300
5	80	33.33	100	400
5	100	39.53	120 48	500
5	120	46.29	140.31	600
5	140	54.01	159.54	700
5	160	63.25	178.17	800
5	180	75	196.15	900
5	200	91.29	213.37	1000
5	220	117.26	229.58	1100
5	240	173.21	244.09	1200
6	0 17	1.16	1.32	1
6	4 17	5 85	9.83	25
6	8.33	8.33	16.22	50
6	12.5	10.28	22 02	75
6	16.67	11.95	27 52	100
6	20.83	13.46	32 82	125
6	25	14.85	37.97	150
6	29.17	16.16	43.01	175
6	33.33	17.41	47.96	200
6	37.5	18.61	52.83	225
6	41.67	19.76	57.63	250
6	50	22	67.08	300
6	66.67	26 26	85.45	400
6	83.33	30.43	103.29	500
6	100	34 64	120.7	600
6	116.67	39.01	137.76	700
6	133.33	43.64	154 5	800
6	150	48.67	170.94	900
6	166.67	54.23	187.08	1000
6	183.33	60.55	202.93	1100
6	200	67.94	218.46	1200
6	216.67	76 87	233.66	1300
6	233.33	88.19	248.48	1400
6	250	103.51	262.83	1500
6	266.67	126.49	276.55	1600
6	283.33	168.33	289.32	1700
6	300	300	300	1800
7	0.14	1	1.14	1
7	3.57	5.03	8.47	25
7	7.14	7.14	14	50
7	10.71	8.79	19.03	75
7	14.29	10.21	23.8	100
7	17.86	11.47	28.4	125

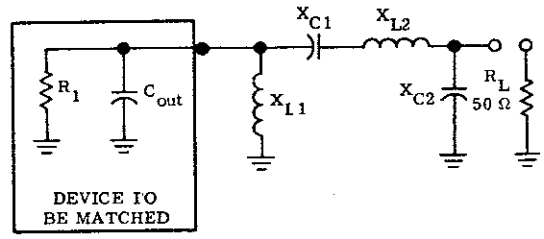
Q	X_{C1}	X_{C2}	X_L	R_1
7	21.43	12.63	32.87	150
7	25	13.72	37.26	175
7	28.57	14.74	41.56	200
7	32.14	15.72	45.81	225
7	35.71	16.67	50	250
7	42.86	18.46	58.25	300
7	57.14	21.82	74.33	400
7	71.43	25	90	500
7	85.71	28.1	105.35	600
7	100	31.18	120.45	700
7	114.29	34.3	135.32	800
7	128.57	37.5	150	900
7	142.86	40.82	164.49	1000
7	171.43	48.04	192.98	1200
7	200	56.41	220.82	1400
7	228.57	66.67	248	1600
7	257.14	80.18	274.45	1800
7	285.71	100	300	2000
7	314.29	135.4	324.25	2200
7	342.86	244.95	345.8	2400
8	0.13	0.88	1	1
8	3.13	4.4	7.45	25
8	6.25	6.25	12.31	50
8	9.38	7.68	16.74	75
8	12.5	8.91	20.94	100
8	15.63	10	25	125
8	18.75	11	28.95	150
8	21.88	11.93	32.82	175
8	25	12.8	36.63	200
8	28.13	13.64	40.38	225
8	31.25	14.43	44.09	250
8	37.5	15.94	51.4	300
8	50	18.73	65.66	400
8	62.5	21.32	79.58	500
8	75	23.79	93.25	600
8	87.5	26.2	106.71	700
8	100	28.57	120	800
8	112.5	30.94	133.14	900
8	125	33.33	146.15	1000
8	150	38.25	171.82	1200
8	175	43.5	197.07	1400
8	200	49.24	221.92	1600
8	225	55.71	246.39	1800
8	250	63.25	270.48	2000
8	275	72.37	294.15	2200
8	300	84.02	317.36	2400
9	8.33	6.83	14.93	75
9	11.11	7.91	18.69	100
9	13.89	8.87	22.32	125
9	16.67	9.74	25.85	150
9	19.44	10.56	29.31	175
9	22.22	11.32	32.72	200
9	25	12.05	36.08	225
9	27.78	12.74	39.4	250
9	33.33	14.05	45.95	300
9	44.44	16.44	58.74	400
9	55.56	18.63	71.24	500
9	66.67	20.7	83.53	600
9	77.78	22.69	95.64	700
9	88.89	24.62	107.62	800
9	100	26.52	119.48	900
9	111.11	28.4	131.23	1000
9	133.33	32.16	154.46	1200
9	155.56	36	177.37	1400
9	177.78	40	200	1600
9	200	44.23	222.37	1800
9	222.22	48.8	244.5	2000
9	244.44	53.8	266.4	2200
9	266.67	59.41	288.05	2400

Q	X_{C1}	X_{C2}	X_L	R_1
10	0.1	0.7	0.8	1
10	5	5	9.9	50
10	10	7.11	16.87	100
10	15	8.75	23.34	150
10	20	10.15	29.55	200
10	25	11.41	35.6	250
10	30	12.57	41.52	300
10	40	14.66	53.11	400
10	50	16.57	64.44	500
10	60	18.36	75.58	600
10	70	20.06	86.58	700
10	80	21.69	97.46	800
10	90	23.28	108.24	900
10	100	24.85	118.94	1000
10	120	27.91	140.09	1200
10	140	30.97	161	1400
10	160	34.05	181.68	1600
10	180	37.21	202.17	1800
10	200	40.49	222.47	2000
10	220	43.93	242.61	2200
10	240	47.58	262.59	2400
12	25	10.39	34.79	300
12	33.33	12.08	44.52	400
12	41.67	13.61	54.05	500
12	50	15.02	63.43	600
12	58.33	16.35	72.7	700
12	66.67	17.61	81.87	800
12	75	18.82	90.97	900
12	83.33	20	100	1000
12	100	22.27	117.89	1200
12	116.67	24.46	135.6	1400
12	133.33	26.61	153.15	1600
12	150	28.73	170.57	1800
12	166.67	30.86	187.86	2000
12	183.33	33	205.06	2200
12	200	35.17	222.15	2400
12	216.67	37.39	239.16	2600
12	233.33	39.66	256.07	2800
12	250	42.01	272.9	3000
12	291.67	48.3	314.64	3500
12	333.33	55.47	355.9	4000
12	375	63.96	396.67	4500
12	416.67	74.54	436.92	5000
12	458.33	88.64	476.57	5500
12	500	109.54	515.44	6000
14	21.43	8.86	29.91	300
14	28.57	10.29	38.3	400
14	35.71	11.56	46.51	500
14	42.86	12.73	54.6	600
14	50	13.83	62.59	700
14	57.14	14.87	70.51	800
14	64.29	15.86	78.37	900
14	71.43	16.81	86.17	1000
14	85.71	18.62	101.63	1200
14	100	20.35	116.95	1400
14	114.29	22.02	132.15	1600
14	128.57	23.64	147.24	1800
14	142.86	25.24	162.25	2000
14	157.14	26.81	177.17	2200
14	171.43	28.38	192.02	2400
14	185.71	29.94	206.81	2600
14	200	31.51	221.54	2800
14	214.29	33.09	236.21	3000
14	250	37.12	272.66	3500
14	285.71	41.34	308.82	4000
14	321.43	45.86	344.7	4500
14	357.14	50.77	380.33	5000
14	392.86	56.22	415.69	5500
14	428.57	62.42	450.79	6000

Q	X_{C1}	X_{C2}	X_L	R_1
16	18.75	7.73	26.23	300
16	25	8.96	33.59	400
16	31.25	10.06	40.8	500
16	37.5	11.07	47.9	600
16	43.75	12	54.93	700
16	50	12.88	61.89	800
16	56.25	13.72	68.79	900
16	62.5	14.52	75.65	1000
16	75	16.05	89.26	1200
16	87.5	17.48	102.74	1400
16	100	18.86	116.12	1600
16	112.5	20.18	129.42	1800
16	125	21.47	142.64	2000
16	137.5	22.73	155.8	2200
16	150	23.96	168.9	2400
16	162.5	25.18	181.95	2600
16	175	26.39	194.96	2800
16	187.5	27.59	207.92	3000
16	218.75	30.59	240.16	3500
16	250	33.61	272.18	4000
16	281.25	36.71	304.01	4500
16	312.5	39.9	335.66	5000
16	343.75	43.25	367.15	5500
16	375	46.8	398.49	6000
18	16.67	6.86	23.35	300
18	22.22	7.94	29.9	400
18	27.78	8.91	36.33	500
18	33.33	9.79	42.66	600
18	38.89	10.61	48.92	700
18	44.44	11.38	55.13	800
18	50	12.11	61.28	900
18	55.56	12.8	67.4	1000
18	66.67	14.12	79.54	1200
18	77.78	15.35	91.57	1400
18	88.89	16.52	103.51	1600
18	100	17.65	115.38	1800
18	111.11	18.73	127.2	2000
18	122.22	19.79	138.95	2200
18	133.33	20.81	150.66	2400
18	144.44	21.82	162.33	2600
18	155.56	22.81	173.96	2800
18	166.67	23.79	185.55	3000
18	194.44	26.2	214.4	3500
18	222.22	28.57	243.08	4000
18	250	30.94	271.6	4500
18	277.78	33.33	300	5000
18	305.56	35.76	328.27	5500
18	333.33	38.25	356.44	6000
20	15	6.16	21.03	300
20	20	7.13	26.94	400
20	25	8	32.73	500
20	30	8.78	38.44	600
20	35	9.51	44.09	700
20	40	10.19	49.69	800
20	45	10.84	55.24	900
20	50	11.46	60.76	1000
20	60	12.62	71.71	1200
20	70	13.7	82.57	1400
20	80	14.72	93.35	1600
20	90	15.7	104.07	1800
20	100	16.64	114.73	2000
20	110	17.55	125.35	2200
20	120	18.44	135.93	2400
20	130	19.3	146.47	2600
20	140	20.14	156.98	2800
20	150	20.97	167.46	3000
20	175	22.99	193.54	3500
20	200	24.96	219.48	4000
20	225	26.9	245.3	4500
20	250	28.82	271.01	5000
20	275	30.74	296.62	5500
20	300	32.67	322.15	6000

NETWORK C_1

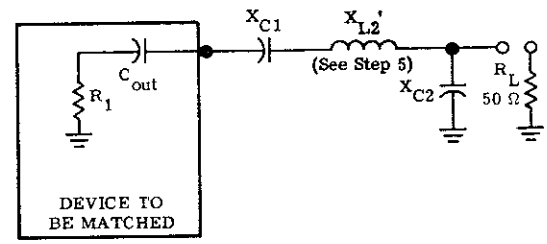
The following is a computer solution for an RF matching network. This computer solution is applicable for two forms of matching networks.



TO DESIGN A NETWORK USING THE TABLES

1. $X_{L1} = X_{C\,out}$
2. Define Q, in column one, as X_{C1}/R_1
3. All network values can now be read from the charts in terms of reactance.
4. This completes network C_1

NETWORK C_2



TO DESIGN A NETWORK USING THE TABLES

1. L_1 is not used in this network
2. Transform the impedance of the device to be matched to series form $(R_1 + jX_{C\,out})$
3. Define Q, in column one, as X_{C1}/R_1
4. For a desired Q, find the R_s to be matched in the R_1 column and read the reactive value of the components
5. X_{L2}' is equal to the quantity X_{L2} obtained from the tables plus $|X_{C_{out}}|$
6. This completes network C_2

Q	X_{C1}	X_{C2}	X_{L2}	R_1
1	1	7.14	8	1
1	2	10.21	11.8	2
1	3	12.63	14.87	3
1	4	14.74	17.56	4
1	5	16.67	20	5
1	6	18.46	22.25	6
1	7	20.17	24.35	7
1	8	21.82	26.33	8
1	9	23.43	28.21	9
1	10	25	30	10
1	11	26.55	31.81	11
1	12	28.1	33.35	12
1	13	29.64	34.93	13
1	14	31.13	36.45	14
1	15	32.73	37.91	15
1	16	34.3	39.32	16
1	17	35.89	40.69	17
1	18	37.5	42	18
1	19	39.14	43.27	19
1	20	40.82	44.49	20
1	21	42.55	45.68	21
1	22	44.32	46.82	22
1	23	46.15	47.92	23
1	24	48.04	48.98	24
1	25	50	50	25
1	26	52.04	50.98	26
1	27	54.17	51.92	27
1	28	56.41	52.82	28
1	29	58.76	53.68	29
1	30	61.24	54.49	30
1	32	66.67	56	32
1	34	72.89	57.32	34
1	36	80.18	58.45	36

Q	X_{C1}	X_{C2}	X_{L2}	R_1
1	38	88.98	59.35	38
1	40	100	60	40
1	42	114.56	60.33	42
1	44	135.4	60.25	44
1	46	169.56	59.56	46
1	48	244.95	57.8	48
2	2	7.14	9	1
2	4	10.21	13.8	2
2	6	12.63	17.87	3
2	8	14.74	21.56	4
2	10	16.67	25	5
2	12	18.46	28.25	6
2	14	20.17	31.35	7
2	16	21.82	34.33	8
2	18	23.43	37.21	9
2	20	25	40	10
2	22	26.55	42.71	11
2	24	28.1	45.35	12
2	26	29.64	47.93	13
2	28	31.18	50.45	14
2	30	32.73	52.91	15
2	32	34.3	55.32	16
2	34	35.89	57.69	17
2	36	37.5	60	18
2	38	39.14	62.27	19
2	40	40.82	64.49	20
2	42	42.55	66.68	21
2	44	44.32	68.82	22
2	46	46.15	70.92	23
2	48	48.04	72.98	24
2	50	50	75	25
2	52	52.04	76.98	26

Q	X_{C1}	X_{C2}	X_{L2}	R_1
2	54	54.17	78.92	27
2	56	56.41	80.82	28
2	58	58.76	82.68	29
2	60	61.24	84.49	30
2	64	66.67	88	32
2	68	72.89	91.32	34
2	72	80.18	94.45	36
2	76	88.98	97.35	38
2	80	100	100	40
2	84	114.56	102.33	42
2	88	135.4	104.25	44
2	92	169.56	105.56	46
2	96	244.95	105.8	48
3	3	7.14	10	1
3	6	10.21	15.8	2
3	9	12.63	20.87	3
3	12	14.74	25.56	4
3	15	16.67	30	5
3	18	18.46	34.25	6
3	21	20.17	38.35	7
3	24	21.82	42.33	8
3	27	23.43	46.21	9
3	30	25	50	10
3	33	26.55	53.71	11
3	36	28.1	57.35	12
3	39	29.64	60.98	13
3	42	31.18	64.45	14
3	45	32.73	67.91	15
3	48	34.3	71.32	16
3	51	35.89	74.69	17
3	54	37.5	78	18
3	57	39.14	81.27	19

Q	X_{C1}	X_{C2}	X_{L2}	R_1
3	60	40.82	84.49	20
3	63	42.55	87.68	21
3	66	44.32	90.82	22
3	69	46.15	93.93	23
3	72	48.04	96.98	24
3	75	50	100	25
3	78	52.04	102.98	26
3	81	54.17	105.92	27
3	84	56.41	108.82	28
3	87	58.76	111.68	29
3	90	61.24	114.49	30
3	96	66.67	120	32
3	102	72.89	125.32	34
3	108	80.18	130.45	36
3	114	88.98	135.35	38
3	120	100	140	40
3	126	114.56	144.33	42
3	132	135.4	148.25	44
3	138	169.56	151.56	46
3	144	244.95	153.8	48
4	4	7.14	11	1
4	8	10.21	17.8	2
4	12	12.63	23.87	3
4	16	14.74	29.56	4
4	20	16.67	35	5
4	24	18.46	40.25	6
4	28	20.17	45.35	7
4	32	21.82	50 33	8
4	36	23.43	55.21	9
4	40	25	60	10
4	44	26.55	64.71	11
4	48	28.1	69.35	12
4	52	29.64	73.93	13
4	56	31.18	78.45	14
4	60	32.73	82.91	15
4	64	34.3	87.32	16
4	68	35.89	91.69	17
4	72	37.5	96	18
4	76	39.14	100.27	19
4	80	40.82	104.49	20
4	84	42.55	108.68	21
4	88	44.32	112.82	22
4	92	46.15	116.92	23
4	96	48.04	120.98	24
4	100	50	125	25
4	104	52.04	128.98	26
4	108	54.17	132.92	27
4	112	56.41	136.82	28
4	116	58.76	140.68	29
4	120	61.24	144.49	30
4	128	66.67	152	32
4	136	72.89	159.32	34
4	144	80.18	166.45	36
4	152	88.98	173.35	38
4	160	100	180	40
4	168	114.56	186.33	42
4	176	135.4	192.25	44
4	184	169.56	197.56	46
4	192	244.95	201.8	48
5	5	7.14	12	1
5	10	10.21	19.8	2
5	15	12.63	26.87	3
5	20	14.74	33.56	4
5	25	16.67	40	5
5	30	18.46	46.25	6
5	35	20.17	52.35	7
5	40	21.82	58.33	8
5	45	23.43	64.21	9
5	50	25	70	10
5	55	26.55	75.71	11

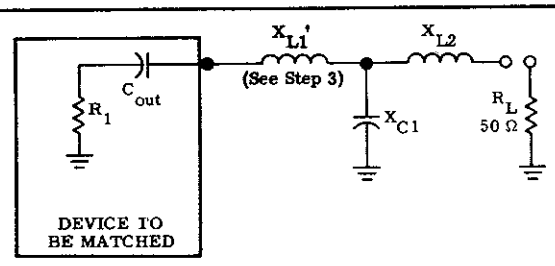
Q	X_{C1}	X_{C2}	X_{L2}	R_1
5	60	28.1	81.35	12
5	65	29.64	86.93	13
5	70	31.18	92.45	14
5	75	32.73	97.91	15
5	80	34.3	103.32	16
5	85	35.89	108.69	17
5	90	37.5	114	18
5	95	39.14	119.27	19
5	100	40.82	124.49	20
5	105	42.55	129.68	21
5	110	44.32	134.82	22
5	115	46.15	139.92	23
5	120	48.04	144.98	24
5	125	50	150	25
5	130	52.04	154.98	26
5	135	54.17	159.92	27
5	140	56.41	164.82	28
5	145	58.76	169.68	29
5	150	61.24	174.49	30
5	160	66.67	184	32
5	170	72.89	193.32	34
5	180	80.18	202.45	36
5	190	88.98	211.35	38
5	200	100	220	40
5	210	114.56	228.33	42
5	220	135.4	236.25	44
5	230	169.56	243.56	46
5	240	244.95	249.8	48
6	6	7.14	13	1
6	12	10.21	21.8	2
6	18	12.63	29.87	3
6	24	14.74	37.56	4
6	30	16.67	45	5
6	36	18.46	52.25	6
6	42	20.17	59.35	7
6	48	21.82	66.33	8
6	54	23.43	73.21	9
6	60	25	80	10
6	66	26.55	86.71	11
6	72	28.1	93.35	12
6	78	29.64	99.93	13
6	84	31.18	106.45	14
6	90	32.73	112.91	15
6	96	34.3	119.32	16
6	102	35.89	125.69	17
6	108	37.5	132	18
6	114	39.14	138.27	19
6	120	40.82	144.49	20
6	126	42.55	150.68	21
6	132	44.32	156.82	22
6	138	46.15	162.92	23
6	144	48.04	168.98	24
6	150	50	175	25
6	156	52.04	180.98	26
6	162	54.17	186.92	27
6	168	56.41	192.82	28
6	174	58.76	198.68	29
6	180	61.24	204.49	30
6	192	66.67	216	32
6	204	72.89	227.32	34
6	216	80.18	238.45	36
6	228	88.98	249.35	38
6	240	100	260	40
6	252	114.56	270.33	42
6	264	135.4	280.25	44
6	276	169.56	289.56	46
6	288	244.95	297.8	48
7	7	7.14	14	1
7	14	10.21	23.8	2
7	21	12.63	32.87	3

Q	X_{C1}	X_{C2}	X_{L2}	R_1
7	28	14.74	41.56	4
7	35	16.67	50	5
7	42	18.46	58.25	6
7	49	20.17	66.35	7
7	56	21.82	74.33	8
7	63	23.43	82.21	9
7	70	25	90	10
7	77	26.55	97.71	11
7	84	28.1	105.35	12
7	91	29.64	112.93	13
7	98	31.18	120.45	14
7	105	32.73	127.91	15
7	112	34.3	135.32	16
7	119	35.89	142.69	17
7	126	37.5	150	18
7	133	39.14	157.27	19
7	140	40.82	164.49	20
7	147	42.55	171.68	21
7	154	44.32	178.82	22
7	161	46.15	185.92	23
7	168	48.04	192.98	24
7	175	50	200	25
7	182	52.04	206.98	26
7	189	54.17	213.92	27
7	196	56.41	220.82	28
7	203	58.76	227.68	29
7	210	61.24	234.49	30
7	224	66.67	248	32
7	238	72.89	261.32	34
7	252	80.18	274.45	36
7	266	88.98	287.35	38
7	280	100	300	40
7	294	114.56	312.33	42
7	308	135.4	324.25	44
7	322	169.56	335.56	46
7	336	244.95	345.8	48
8	8	7.14	15	1
8	16	10.21	25.8	2
8	24	12.63	35.87	3
8	32	14.74	45.56	4
8	40	16.67	55	5
8	48	18.46	64.25	6
8	56	20.17	73.35	7
8	64	21.82	82.33	8
8	72	23.43	91.21	9
8	80	25	100	10
8	88	26.55	108.71	11
8	96	28.1	117.35	12
8	104	29.64	125.93	13
8	112	31.18	134.45	14
8	120	32.73	142.91	15
8	128	34.3	151.32	16
8	136	35.89	159.69	17
8	144	37.5	168	18
8	152	39.14	176.27	19
8	160	40.82	184.49	20
8	168	42.55	192.68	21
8	176	44.32	200.82	22
8	184	46.15	208.92	23
8	192	48.04	216.98	24
8	200	50	225	25
8	208	52.04	232.98	26
8	216	54.17	240.92	27
8	224	56.41	248.82	28
8	232	58.76	256.68	29
8	240	61.24	264.49	30
8	256	66.67	280	32
8	272	72.89	295.32	34
8	288	80.18	310.45	36
8	304	88.98	325.35	38

Q	X_{C1}	X_{C2}	X_{L2}	R_1
8	320	100	340	40
8	336	114.56	354.33	42
8	352	135.4	368.25	44
8	368	169.56	381.56	46
8	384	244.95	393.8	48
9	9	7.14	16	1
9	18	10.21	27.8	2
9	27	12.63	38.87	3
9	36	14.74	49.56	4
9	45	16.67	60	5
9	54	18.46	70.25	6
9	63	20.17	80.35	7
9	72	21.82	90.33	8
9	81	23.43	100.21	9
9	90	25	110	10
9	99	26.55	119.71	11
9	108	28.1	129.35	12
9	117	29.64	138.93	13
9	126	31.18	148.45	14
9	135	32.73	157.91	15
9	144	34.3	167.32	16
9	153	35.89	176.69	17
9	162	37.5	186	18
9	171	39.17	195.27	19
9	180	40.82	204.49	20
9	189	42.55	213.68	21
9	198	44.32	222.82	22
9	207	46.15	231.92	23
9	414	169.56	427.56	46
9	432	244.95	441.8	48
9	216	48.04	240.98	24
9	225	50	250	25
9	234	52.04	258.98	26
9	243	54.17	267.92	27
9	252	56.41	276.82	28
9	261	58.76	285.88	29
9	270	61.24	294.49	30
9	288	66.67	312	32
9	306	72.89	329.32	34
9	324	80.18	346.45	36
9	342	88.98	363.35	38
9	360	100	380	40
9	378	114.56	396.33	42
9	396	135.4	412.25	44
10	10	7.14	17	1
10	20	10.21	29.8	2
10	30	12.63	41.87	3
10	40	14.74	53.56	4
10	50	16.67	65	5
10	60	18.46	76.25	6
10	70	20.17	87.35	7
10	80	21.82	98.33	8
10	90	23.43	109.21	9
10	100	25	120	10
10	110	26.55	130.71	11
10	120	28.1	141.35	12
10	130	29.64	151.93	13
10	140	31.18	162.45	14
10	150	32.73	172.91	15
10	160	34.3	183.32	16
10	170	35.89	193.69	17
10	180	37.5	204	18
10	190	39.14	214.27	19
10	200	40.82	224.49	20
10	210	42.55	234.68	21
10	220	44.32	244.82	22
10	230	46.15	254.92	23
10	240	48.04	264.98	24
10	250	50	275	25
10	260	52.04	284.98	26
10	270	54.17	294.92	27
10	280	56.41	304.82	28
10	290	58.76	314.68	29
10	300	61.24	324.49	30
10	320	66.67	344	32
10	340	72.89	363.32	34
10	360	80.18	382.45	36
10	380	88.98	401.35	38
10	400	100	420	40
10	420	114.56	438.33	42
10	440	135.4	456.25	44
10	460	169.56	473.56	46
10	480	244.95	489.8	48

NETWORK D

The following is a computer solution for an RF "Tee" matching network.
Tuning is accomplished by using a variable capacitor for C_1. Variable matching may also be accomplished by increasing X_{L2} and adding an equal amount of X_C in series in the form of a variable capacitor.



TO DESIGN A NETWORK USING THE TABLES

1. Define Q, in column one, as X_{L1}/R_1.
2. For an R_1 to be matched and a desired Q, read the reactances of the network components from the charts.
3. X_{L1}' is equal to the quantity X_{L1} obtained from the tables plus $|X_{C_{out}}|$.
4. This completes the network.

Q	X_{L1}	X_{L2}	X_{C1}	R_1
1	26	10	43.33	26
1	27	14.14	42.09	27
1	28	17.32	41.59	28
1	29	20	41.43	29
1	30	22.36	41.46	30
1	32	26.46	41.85	32
1	34	30	42.5	34
1	36	33.17	43.29	36
1	38	36.06	44.16	38
1	40	38.72	45.08	40
1	42	41.23	46.04	42
1	44	43.59	47.01	44
1	46	45.83	48	46
1	48	47.96	49	48
1	50	50	50	50
1	55	54.77	52.49	55
1	60	59.16	54.96	60
1	65	63.25	57.4	65
1	70	67.08	69.79	70
1	75	70.71	62.13	75
1	80	74.16	64.43	80
1	85	77.46	66.69	85
1	90	80.62	68.9	90
1	95	83.67	71.07	95
1	100	86.6	73.21	100
1	125	100	83.33	125
1	150	111.8	92.71	150
1	175	122.47	101.46	175
1	200	132.29	109.72	200
1	225	141.42	117.54	225
1	250	150	125	250
1	275	158.11	132.14	275
1	300	165.83	139	300
2	22	15.81	23.75	11
2	24	22.36	24.52	12
2	26	27.39	25.51	13
2	28	31.62	26.59	14
2	30	35.36	27.7	15
2	32	38.73	28.83	16
2	34	41.83	29.96	17
2	36	44.72	31.09	18
2	38	47.43	32.22	19
2	40	50	33.33	20
2	42	52.44	34.44	21
2	44	54.77	35.54	22
2	46	57.01	36.62	23
2	48	59.16	37.7	24
2	50	61.24	38.76	25
2	52	63.25	39.82	26
2	54	65.19	40.86	27
2	56	67.08	41.9	28
2	58	68.92	42.92	29
2	60	70.71	43.93	30
2	64	74.16	45.93	32
2	68	77.46	47.9	34
2	72	80.62	49.83	36
2	76	83.67	51.72	38
2	80	86.6	53.59	40
2	84	89.44	55.43	42
2	88	92.2	57.23	44
2	92	94.87	59.01	46
2	96	97.47	60.77	48
2	100	100	62.5	50
2	110	106.07	66.73	55
2	120	111.8	70.82	60
2	130	117.26	74.8	65
2	140	122.47	78.66	70
2	150	127.48	82.43	75
2	160	132.29	86.1	80
2	170	136.93	89.69	85
2	180	141.42	93.2	90
2	190	145.77	96.63	95
2	200	150	100	100
2	250	169.56	115.93	125
2	300	187.08	130.62	150
2	350	203.1	144.34	175
2	400	217.94	157.26	200
2	450	231.84	169.51	225
2	500	244.95	181.19	250
2	550	257.39	192.37	275
2	600	269.26	203.11	300

Q	X_{L1}	X_{L2}	X_{C1}	R_1
3	18	22.36	17.41	6
3	21	31.62	19.27	7
3	24	38.73	21.19	8
3	27	44.72	23.11	9
3	30	50	25	10
3	33	54.77	26.86	11
3	36	59.16	28.69	12
3	39	63.25	30.48	13
3	42	67.08	32.25	14
3	45	70.71	33.98	15
3	48	74.16	35.69	16
3	51	77.46	37.37	17
3	54	80.62	39.02	18
3	57	83.67	40.66	19
3	60	86.6	42.26	20
3	63	89.44	43.85	21
3	66	92.2	45.42	22
3	69	94.87	46.96	23
3	72	97.47	48.49	24
3	75	100	50	25
3	78	102.47	51.49	26
3	81	104.88	52.97	27
3	84	107.24	54.42	28
3	87	109.54	55.87	29
3	90	111.8	57.29	30
3	96	116.19	60.11	32
3	102	120.42	62.87	34
3	108	124.5	65.57	36
3	114	128.45	68.23	38
3	120	132.29	70.85	40
3	126	136.01	73.42	42
3	132	139.64	75.96	44
3	138	143.18	78.45	46
3	144	146.63	80.91	48
3	150	150	83.33	50
3	165	158.11	89.25	55
3	180	165.83	94.99	60
3	195	173.21	100.56	65
3	210	180.28	105.97	70
3	225	187.08	111.25	75
3	240	193.65	116.4	80
3	255	200	121.43	85
3	270	206.16	126.35	90
3	285	212.13	131.17	95
3	300	217.94	135.89	100
3	375	244.95	158.25	125
3	450	269.26	178.89	150
3	525	291.55	198.17	175
3	600	312.25	216.33	200
3	675	331.66	233.57	225
3	750	350	250	250
3	825	367.42	265.74	275
3	900	384.06	280.87	300
4	12	7.07	12.31	3
4	16	30	14.78	4
4	20	41.83	17.57	5
4	24	50.99	20.32	6
4	28	58.74	23	7
4	32	65.57	25.6	8
4	36	71.76	28.15	9
4	40	77.46	30.64	10
4	44	82.76	33.07	11
4	48	87.75	35.45	12
4	52	92.47	37.78	13
4	56	96.95	40.07	14
4	60	101.24	42.32	15
4	64	105.36	44.54	16
4	68	109.32	46.72	17
4	72	113.14	48.86	18
4	76	116.83	50.97	19
4	80	120.42	53.06	20
4	84	123.9	55.11	21
4	88	127.28	57.14	22
4	92	130.58	59.14	23
4	96	133.79	61.12	24
4	100	136.93	63.07	25
4	104	140	65	26
4	108	143	66.91	27

Q	X_{L1}	X_{L2}	X_{C1}	R_1
4	112	145.95	68.8	28
4	116	148.83	70.67	29
4	120	151.66	72.51	30
4	128	157.16	76.16	32
4	136	162.48	79.73	34
4	144	167.63	83.24	36
4	152	172.63	86.68	38
4	160	177.48	90.07	40
4	168	182.21	93.4	42
4	176	186.82	96.69	44
4	184	191.31	99.92	46
4	192	195.7	103.11	48
4	200	200	106.25	50
4	220	210.36	113.93	55
4	240	220.23	121.36	60
4	260	229.67	128.59	65
4	280	238.75	135.61	70
4	300	247.49	142.46	75
4	320	255.93	148.15	80
4	340	264.1	155.68	85
4	360	272.03	162.07	90
4	380	279.73	168.32	95
4	400	287.23	174.46	100
4	500	322.1	203.5	125
4	600	353.55	230.33	150
4	700	382.43	255.4	175
4	800	409.27	279.02	200
4	900	434.45	301.44	225
4	1000	458.26	322.82	250
4	1100	480.88	343.3	275
4	1200	502.49	362.99	300
5	10	10	10	2
5	15	37.42	13.57	3
5	20	51.96	17.22	4
5	25	63.25	20.75	5
5	30	72.8	24.16	6
5	35	81.24	27.47	7
5	40	88.88	30.69	8
5	45	95.92	33.82	9
5	50	102.47	36.88	10
5	55	108.63	39.87	11
5	60	114.46	42.8	12
5	65	120	45.68	13
5	70	125.3	48.49	14
5	75	130.38	51.26	15
5	80	135.28	53.99	16
5	85	140	56.67	17
5	90	144.57	59.31	18
5	95	149	61.91	19
5	100	153.3	64.47	20
5	105	157.48	67	21
5	110	161.55	69.49	22
5	115	165.53	71.96	23
5	120	169.41	74.39	24
5	125	173.21	76.79	25
5	130	176.92	79.17	26
5	135	180.55	81.52	27
5	140	184.12	83.85	28
5	145	187.62	86.15	29
5	150	191.05	88.43	30
5	160	197.74	92.91	32
5	170	204.21	97.31	34
5	180	210.48	101.63	36
5	190	216.56	105.88	38
5	200	222.49	110.06	40
5	210	228.25	114.17	42
5	220	233.88	118.21	44
5	230	239.37	122.2	46
5	240	244.74	126.13	48
5	250	260	130	50
5	275	262.68	139.46	55
5	300	274.77	148.64	60
5	325	286.36	157.54	65
5	350	297.49	166.21	70
5	375	308.22	174.66	75
5	400	318.59	182.91	80
5	425	328.63	190.97	85
5	450	338.38	198.85	90
5	475	347.85	206.57	95
5	500	357.07	214.14	100

Q	X_{L1}	X_{L2}	X_{C1}	R_1
5	625	400	250	125
5	750	438.75	283.12	150
5	875	474.34	314.08	175
5	1000	507.44	343.26	200
5	1125	538.52	670.95	225
5	1250	567.89	397.36	250
5	1375	595.82	422.67	275
5	1500	622.49	446.99	300
6	12	34.64	11.06	2
6	18	55.23	15.62	3
6	24	70	20	4
6	30	82.16	24.2	5
6	36	92.74	28.26	6
6	42	102.23	32.2	7
6	48	110.91	36.02	8
6	54	118.95	39.74	9
6	60	126.49	43.38	10
6	66	133.6	46.93	11
6	72	140.36	50.41	12
6	78	146.8	53.83	13
6	84	152.97	57.18	14
6	90	158.9	60.47	15
6	96	164.62	63.71	16
6	102	170.15	66.89	17
6	108	175.5	70.03	18
6	114	180.69	73.12	19
6	120	185.74	76.17	20
6	126	190.66	79.18	21
6	132	195.45	82.15	22
6	138	200.12	85.08	23
6	144	204.69	87.97	24
6	150	209.17	90.83	25
6	156	213.54	93.66	26
6	162	217.83	96.46	27
6	168	222.04	99.23	28
6	174	226.16	101.96	29
6	180	230.22	104.67	30
6	192	238.12	110.01	32
6	204	245.76	115.25	34
6	216	253.18	120.39	36
6	228	260.38	125.45	38
6	240	267.39	130.42	40
6	252	274.23	135.31	42
6	264	280.89	140.13	44
6	276	287.4	144.88	46
6	288	293.77	149.55	48
6	300	300	154.17	50
6	330	315.04	165.44	55
6	360	329.39	176.36	60
6	390	343.15	186.97	65
6	420	356.37	197.3	70
6	450	369.12	207.36	75
6	480	381.44	217.19	80
6	510	393.38	226.79	85
6	540	404.97	236.18	90
6	570	416.23	245.38	95
6	600	427.2	254.4	100
6	750	478.28	297.13	125
6	900	524.4	336.61	150
6	1050	566.79	373,5	175
6	1200	606.22	408.29	200
6	1350	643.23	441.3	225
6	1500	678.23	472.79	250
6	1650	711.51	502.96	275
6	1800	743.3	531.96	300
7	14	50	12.5	2
7	21	70.71	17.83	3
7	28	86.6	22.9	4
7	35	100	27.78	5
7	42	111.8	32.48	6
7	49	122.47	37.04	7
7	56	132.29	41.47	8
7	63	141.42	45.79	9
7	70	150	50	10
7	77	158.11	54.12	11
7	84	165.83	58.16	12
7	91	173.21	62.12	13
7	98	180.28	66	14
7	105	187.08	69.82	15
7	112	193.65	73.58	16

Q	X_{L1}	X_{L2}	X_{C1}	R_1
7	119	200	77.27	17
7	126	206.16	80.91	18
7	133	212.13	84.5	19
7	140	217.94	88.04	20
7	147	223.61	91.53	21
7	154	229.13	94.97	22
7	161	234.52	98.37	23
7	168	239.79	101.73	24
7	175	244.95	105.05	25
7	182	250	108.33	26
7	189	254.95	111.58	27
7	196	259.81	114.79	28
7	203	264.58	117.97	29
7	210	269.26	121.11	30
7	224	278.39	127.31	32
7	238	287.23	133.39	34
7	252	295.8	139.36	36
7	266	304.14	145.23	38
7	280	312.25	151	40
7	294	320.16	156.68	42
7	308	327.87	162.27	44
7	322	335.41	167.78	46
7	336	342.78	173.21	48
7	350	350	178.57	50
7	385	367.42	191.66	55
7	420	384.06	204.34	60
7	455	400	216.67	65
7	490	415.33	228.66	70
7	525	430.12	240.35	75
7	560	444.41	251.76	80
7	595	458.86	262.91	85
7	630	471.7	273.82	90
7	665	484.77	284.51	95
7	700	497.49	294.99	100
7	875	556.78	344.63	125
7	1050	610.33	390.49	150
7	1225	659.55	433.36	175
7	1400	705.34	473.78	200
7	1575	748.33	512.14	225
7	1750	788.99	548.73	250
7	1925	827.65	583.79	275
7	2100	864.58	617.5	300
8	8	27.39	7.6	1
8	16	63.25	14.03	2
8	24	85.15	20.1	3
8	32	102.47	25.87	4
8	40	117.26	31.42	5
8	48	130.38	36.77	6
8	56	142.3	41.95	7
8	64	153.3	46.99	8
8	72	163.55	51.9	9
8	80	173.21	56.7	10
8	88	182.35	61.39	11
8	96	191.05	65.98	12
8	104	199.37	70.49	13
8	112	207.36	74.91	14
8	120	215.06	79.26	15
8	128	222.49	83.54	16
8	136	229.67	87.74	17
8	144	236.64	91.89	18
8	152	243.41	95.97	19
8	160	250	100	20
8	168	256.42	103.97	21
8	176	262.68	107.9	22
8	184	268.79	111.77	23
8	192	274.77	115.59	24
8	200	280.62	119.38	25
8	208	286.36	123.11	26
8	216	291.98	126.81	27
8	224	297.49	130.47	28
8	232	302.9	134.09	29
8	240	308.22	137.67	30

Q	X_{L1}	X_{L2}	X_{C1}	R_1
8	256	318.59	144.73	32
8	272	328.63	151.65	34
8	288	338.38	158.46	36
8	304	347.85	165.14	38
8	320	357.07	171.71	40
8	336	366.06	178.18	42
8	352	374.83	184.56	44
8	368	383.41	190.83	46
8	384	391.79	197.02	48
8	400	400	203.13	50
8	440	419.82	218.04	55
8	480	438.75	232.49	60
8	520	456.89	246.53	65
8	560	474.34	260.2	70
8	600	491.17	273.52	75
8	640	507.44	286.52	80
8	680	523.21	299.23	85
8	720	538.52	311.66	90
8	760	553.4	323.84	95
8	800	567.89	335.78	100
8	1000	635.41	392.36	125
8	1200	696.42	444.63	150
8	1400	752.5	493.49	175
8	1600	804.67	539.57	200
8	1800	853.67	583.29	225
8	2000	900	625	250
8	2200	944.06	664.96	275
8	2400	986.15	703.38	300
9	9	40	8.37	1
9	18	75.5	15.6	2
9	27	98.99	22.4	3
9	36	117.9	28.88	4
9	45	134.16	35.09	5
9	54	148.66	41.09	6
9	63	161.86	46.91	7
9	72	174.07	52.56	8
9	81	185.47	58.07	9
9	90	196.21	63.45	10
9	99	206.4	68.71	11
9	108	216.1	73.86	12
9	117	225.39	78.92	13
9	126	234.31	83.88	14
9	135	242.9	88.76	15
9	144	251.2	93.55	16
9	153	259.23	98.28	17
9	162	267.02	102.93	18
9	171	274.59	107.51	19
9	180	281.96	112.03	20
9	189	289.14	116.49	21
9	198	296.14	120.89	22
9	207	302.99	125.23	23
9	216	309.68	129.53	24
9	225	316.23	133.77	25
9	234	322.65	137.97	26
9	243	328.94	142.12	27
9	252	335.11	146.22	28
9	261	341.17	150.28	29
9	270	347.13	154.3	30
9	288	358.75	162.23	32
9	306	370	170	34
9	324	380.92	177.63	36
9	342	391.54	185.14	38
9	360	401.87	192.52	40
9	378	411.95	199.78	42
9	396	421.78	206.93	44
9	414	431.39	213.98	46
9	432	440.79	220.93	48
9	450	450	227.78	50
9	495	472.23	244.52	55
9	540	493.46	260.74	60
9	585	513.81	276.51	65
9	630	533.39	291.85	70

Q	X_{L1}	X_{L2}	X_{C1}	R_1
9	675	552.27	306.8	75
9	720	570.53	321.4	80
9	765	588.22	335.67	85
9	810	605.39	349.63	90
9	855	622.09	363.31	95
9	900	638.36	376.71	100
9	1125	714.14	440.24	125
9	1350	782.62	498.94	150
9	1575	845.58	553.81	175
9	1800	904.16	605.54	200
9	2025	959.17	654.64	225
9	2250	1011.19	701.48	250
9	2475	1060.66	746.36	275
9	2700	1107.93	789.51	300
10	10	50.5	9.17	1
10	20	87.18	17.2	2
10	30	112.47	24.74	3
10	40	133.04	31.91	4
10	50	150.83	38.8	5
10	60	166.73	45.45	6
10	70	181.25	51.89	7
10	80	194.68	58.16	8
10	90	207.24	64.26	9
10	100	219.09	70.23	10
10	110	230.33	76.06	11
10	120	241.04	81.78	12
10	130	251.3	87.38	13
10	140	261.15	92.89	14
10	150	270.65	98.29	15
10	160	279.82	103.61	16
10	170	288.7	108.85	17
10	180	297.32	114.01	18
10	190	305.7	119.09	19
10	200	313.85	124.1	20
10	210	321.79	129.05	21
10	220	329.55	133.93	22
10	230	337.12	138.75	23
10	240	344.53	143.51	24
10	250	351.78	148.22	25
10	260	358.89	152.87	26
10	270	365.86	157.47	27
10	280	372.69	162.03	28
10	290	379.41	166.53	29
10	300	386.01	170.99	30
10	320	398.87	179.78	32
10	340	411.34	188.4	34
10	360	423.44	196.87	36
10	380	435.2	205.2	38
10	400	446.65	213.38	40
10	420	457.82	221.44	42
10	440	468.72	229.37	44
10	460	479.37	237.19	46
10	480	489.8	244.9	48
10	500	500	252.5	50
10	550	524.64	271.07	55
10	600	548.18	289.07	60
10	650	570.75	306.56	65
10	700	592.45	323.58	70
10	750	613.39	340.18	75
10	800	633.64	356.37	80
10	850	653.26	372.21	85
10	900	672.31	387.7	90
10	950	690.83	402.87	95
10	1000	708.87	417.74	100
10	1250	792.94	488.23	125
10	1500	868.91	553.36	150
10	1750	938.75	614.25	175
10	2000	1003.74	671.66	200
10	2250	1064.78	726.14	225
10	2500	1122.5	778.12	250
10	2750	1177.39	827.92	275
10	3000	1229.84	875.8	300