

# Designer heat sinks

Using two worked examples, Ray Fautley shows how quick and easy it is to determine heat sink size for any transistor or diode using a design table.

**S**emiconductor devices need to be mounted on metal panels of sufficient size and thermal conductivity to be able to conduct excessive heat away from the junction of the transistor or diode. This is necessary to prevent the temperature of the device's junction from exceeding its maximum rating.

The total thermal path between the device junction and the ambient temperature existing inside the case of the equipment is measured as a thermal resistance. It is referred to as  $R_{th(j-amb)}$ , or as  $\theta_{(j-a)}$ . This term that is easy to assess. You

only need to know three things. One is the maximum allowable junction temperature – which for most discrete silicon devices may be assumed to be about 200°C. Secondly you need to know the ambient temperature, which, inside electronic equipment is usually about 50°C, and finally you need to know the power dissipated in the semiconductor.

This total thermal path  $R_{th(j-amb)}$  comprises three parts,

- The thermal path from device function to its case,  $R_{th(j-c)}$ , also called  $\theta_{th(j-c)}$  or  $R_{th(j-mb)}$ .
- The thermal path between the case of the device and the heat-sink to which it is fitted,  $R_{th(c-hs)}$ , also called  $\theta_{th(c-hs)}$ .
- The thermal path between the heat-sink and the ambient temperature inside the equipment,  $R_{th(hs-amb)}$ , or  $\theta_{(h-a)}$ .

All of these three paths – and of course, the total path  $R_{th(j-amb)}$  are measured in °C/W. This makes the total thermal path  $R_{th(j-amb)} = R_{th(j-c)} + R_{th(c-hs)} + R_{th(hs-amb)}$ .

The first of the three terms,  $R_{th(j-c)}$ , can be found in the data sheets provided by the manufacturer of the semiconductor device.

Path  $R_{th(c-hs)}$  depends on the method used to mount the

transistor or diode to the heat-sink. In some cases the device may be mounted directly on to the heat-sink, but in others it may be necessary to provide some form of electrical insulation between the device and the heat-sink.

Unfortunately, electrical insulation also means some degree of heat insulation so a compromise is necessary. A thin mica washer can provide the electrical insulation. As the semiconductor's working voltage does not exceed a few tens of volts, a thick insulator is unnecessary.

Heat conduction is assisted by the use of silicon grease between the surfaces. Path  $R_{th(c-hs)}$  can be considered to be between 0.1 and 0.7°C/W. In practice, a value of 0.4°C/W is usually acceptable for this term. This leaves the third term,  $R_{th(hs-amb)}$ , which needs to be evaluated.

## Heat sink design steps

1. From the semiconductor data sheet, find  $R_{th(j-c)}$  in °C/W.
2. Determine  $R_{th(c-hs)}$  in °C/W. This value depends on the effectiveness of the thermal contact between the case of the semiconductor and the surface of the heat-sink. A value of 0.4°C/W will be a good enough approximation if the actual value is unknown.
3. Determine the power dissipated in the device,

(a) For power-amplifier transistors the power dissipated is,

$$P_D = P_{in} - P_{out} \\ = V_{ce} \times I_c - P_{ac}$$

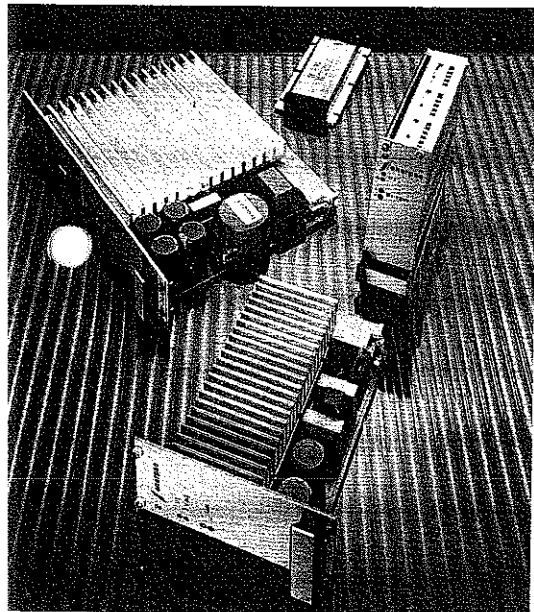
(b) For rectifier diodes,

$$P_D = V_D - I_{ave}$$

4. Find,

$$R_{th(j-amb)} = \frac{T_j - T_{amb}}{P_D} \text{ in } ^\circ\text{C/W}$$

For silicon devices, maximum junction temperature  $T_j$  is usually 200°C, but to be safe it is better to design around 150°C. In some cases  $T_j$  may be specified lower than 200°C, so always check with the manufacturer's data before proceeding with the heat-sink design. Inside the equipment, the ambient temperature  $T_{amb}$  can be assumed to be 50°C.



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5. Determine,

$$R_{th(hs-amb)} = R_{th(j-amb)} - R_{th(j-c)} - R_{th(c-hs)}$$

6. The surface area of the heat-sink required to provide the necessary  $R_{th(hs-amb)}$  can be found from **Table 1**.

A variation of the thickness of the heat-sink between 1mm and 5mm does not have very much effect. It is surface area that counts. These figures should provide adequate design margins.

Note that the surface areas in the table are for one side of the heat-sink only, the total surface area is thus twice the table figure – plus twice the thickness of the metal.

All heat-sink surfaces are assumed to be painted matt-black and mounted horizontally. Vertical mounting increases the cooling effect and adds a further margin of safety. But bright metal surfaces will need the figures of Table 1 to be increased by some 33%.

Note that the figures were arrived by experimentation. After comparing various results using different methods for arriving at the necessary surface area for the same value of  $R_{th(hs-amb)}$ , agreement was not 100%.

**Design examples**

These two worked examples should help clarify the design procedure for you.

**Example 1.** A rectifier diode, for which the manufacturer's data gives  $R_{th(j-c)} = 5^\circ\text{C/W}$ , has a forward voltage drop 1.0V when the average current through it – or dc load – is 5A. The maximum junction temperature  $T_j$  of the diode is given as  $100^\circ\text{C}$ . Inside the equipment that the rectifier is to be used in, the ambient temperature will be assumed to be  $50^\circ\text{C}$ .

**Design procedure**

1.  $R_{th(j-c)}$  is known to be  $5^\circ\text{C/W}$ .
2. Assume that  $R_{th(c-hs)}$  will be  $0.4^\circ\text{C/W}$ .
3. Power dissipated in the diode is,

$$P_d = V_d \times I_{ave} = 1.0 \times 5 = 5\text{W for a } T_j \text{ of } 100^\circ\text{C}$$

$$4. R_{th(j-amb)} = \frac{T_j - T_{amb}}{P_d} = \frac{100 - 50}{5} = \frac{50}{5} = 10^\circ\text{C/W}$$

$$5. R_{th(hs-amb)} = R_{th(j-amb)} - R_{th(j-c)} - R_{th(c-hs)} = 10 - 5 - 0.4 = 4.6^\circ\text{C/W}$$

6. Referring to Table 1 gives the following dimensions for a suitable heat-sink.

- For copper,  $84\text{cm}^2$  or  $9.2\text{cm} \times 9.2\text{cm}$
- For aluminium,  $100\text{cm}^2$  or  $10\text{cm} \times 10\text{cm}$
- For brass,  $113\text{cm}^2$  or  $10.6\text{cm} \times 10.6\text{cm}$
- For steel,  $128\text{cm}^2$  or  $11.3\text{cm} \times 11.3\text{cm}$

**Example 2.**

A *BLW81* transistor is to be used as a vhf power amplifier to provide a cw output of 10W.

**Design procedure**

1. The thermal resistance from junction to case  $R_{th(j-c)}$  is given by its manufacturer as  $4.3^\circ\text{C/W}$ .
2. Say  $R_{th}$  is  $0.4^\circ\text{C/W}$ .
3. Efficiency of the *BLW81* is given as about 60% as a cw

**Heat sink terms**

Term	Description	Units
$I_{ave}$	Average current through diode	A dc
$I_c$	Transistor collector current	A dc
$P_D$	Power dissipated in transistor.	W
$P_{in}$	Power input to device, dc	W
$P_{out}$	Output power – rf or af from transistor	W
$R_{th(c-hs)}$	Thermal resistance between device case and heat-sink	$^\circ\text{C/W}$
$R_{th(hs-amb)}$	Thermal resistance between heat-sink and $T_{amb}$	$^\circ\text{C/W}$
$R_{th(j-amb)}$	Thermal resistance between device junction and $T_{amb}$	$^\circ\text{C/W}$
$R_{th(j-c)}$	Thermal resistance between device junction and case	$^\circ\text{C/W}$
$T_{amb}$	Ambient temperature inside equipment	$^\circ\text{C}$
$T_j$	Maximum temperature of device junction	$^\circ\text{C}$
$V_{ce}$	Potential between collector and emitter of device	V
$V_d$	Voltage drop across diode at stated current	V dc

amplifier, so the input power for 10W output will be,

$$P_{in} = \frac{P_{out}}{0.6} = \frac{10}{0.6} = 16.7\text{W}$$

So,

$$P_D = P_{in} - P_{out} = 16.7 - 10 = 6.7\text{W}.$$

$$4. R_{th(j-amb)} = \frac{T_j - T_{amb}}{P_D} = \frac{150 - 50}{6.7} = 14.9^\circ\text{C/W}$$

$$5. R_{th(hs-amb)} = R_{th(j-amb)} - R_{th(j-c)} - R_{th(c-hs)} = 14.9 - 4.3 - 0.4 = 10.2^\circ\text{C/W}$$

6. From Table 1, suitable heat-sinks are,  
 For copper,  $29\text{cm}^2$  or  $5.4\text{cm} \times 5.4\text{cm}$   
 For aluminium,  $35\text{cm}^2$  or  $5.9\text{cm} \times 5.9\text{cm}$   
 For brass,  $37\text{cm}^2$  or  $6.4\text{cm} \times 6.4\text{cm}$   
 For steel,  $130\text{cm}^2$  or  $11.4\text{cm} \times 11.4\text{cm}$

My thanks to Anglia Microwaves of Billericay, Essex for their help in providing semiconductor data.

**Table 1. These figures give you the surface area in  $\text{cm}^2$  for one side of the heat sink for a known value of  $R_{th(hs-amb)}$ .**

$R_{th(hs-amb)}$ $^\circ\text{C/W}$	Material			
	Copper	Aluminium	Brass	Steel
1	734	—	—	—
1.5	342	—	—	—
2	220	376	477	—
2.5	175	277	302	711
3	135	187	210	338
3.5	116	149	175	222
4	94	120	150	165
4.5	85	102	115	132
5	70	83	90	109
6	53	68	72	82
7	41	61	63	66
8	37	55	58	61
9	33	39	44	47
10	29	35	37	41
11	26	30	33	36
12	24	29	30	32
13	22	27	29	30
14	20	25	26	27
20	14	17	18	20